

Description	
Wall:	SW1
Span:	Section 1 - (7.00-10.50)
Segment:	S1
Concrete:	35.00 MPa
Steel for horizontal reinforcement:	420.00 MPa
Steel for vertical reinforcement:	420.00 MPa

ACI 318M-14, Work section 11

### In-plane shear strength (ACI 318M-14, 11.5.4)

The worst case forces to be withstood from the analysis are produced at Elevation 7.00 (Base), in the combination of loadcase 0.9·PP+0.9·CM+0.3·SX+SY.

$$\phi V_n \geq V_u \quad 2382.0 \text{ kN} \geq 1621.2 \text{ kN} \quad \checkmark$$

Where:

$V_u$ : Factored shear force at section.

$$V_u : \underline{1621.2} \text{ kN}$$

$V_n$ : Nominal shear strength.

$$V_n : \underline{3970.0} \text{ kN}$$

$$V_n = V_c + V_s$$

$$V_n \leq 0.83\sqrt{f'_c}hd$$

$V_c$ : Nominal shear strength provided by concrete.

$$V_c : \underline{2524.8} \text{ kN}$$

$$V_c = \text{MIN}(V_{c1}, V_{c2})$$

$$V_{c1} = 0.27\lambda\sqrt{f'_c}hd + \frac{N_u d}{4l_w}$$

$$V_{c1} : \underline{2524.8} \text{ kN}$$

$$V_{c2} = \left[ 0.05\lambda\sqrt{f'_c} + \frac{l_w \left( 0.1\lambda\sqrt{f'_c} + 0.2 \frac{N_u}{l_w h} \right)}{\frac{M_u}{V_u} - \frac{l_w}{2}} \right] hd$$

$$V_{c2} : \underline{12356.8} \text{ kN}$$

$V_s$ : Nominal shear strength provided by shear reinforcement.

$$V_s : \underline{1445.2} \text{ kN}$$

$$V_s = \frac{A_v f_y d}{s}$$

$N_u$ : Factored axial force.

$$N_u : \underline{3040.0} \text{ kN}$$

$M_u$ : Factored moment.

$$M_u : \underline{-4861.1} \text{ kN}\cdot\text{m}$$

$A_v/s$ : Area of shear reinforcement.

$$A_v/s : \underline{8.60} \text{ cm}^2/\text{m}$$

$f'_c$ : Specified compressive strength of concrete.

$$f'_c : \underline{35.00} \text{ MPa}$$

$$\sqrt{f'_c} \leq 8.3 \text{ MPa}$$

$f_y$ : Specified yield strength of transverse reinforcement.

$$f_y : \underline{420.00} \text{ MPa}$$

$l_w$ : Length of wall.

$$l_w : \underline{500.0} \text{ cm}$$

$h$ : Thickness of wall.

$$h : \underline{30.0} \text{ cm}$$

$d$ : Distance from extreme compression fiber to centroid of longitudinal tension reinforcement.

$$d : \underline{400.0} \text{ cm}$$

$$d = 0.8 \cdot l_w$$

$l$ : Modification factor to reflect the reduced mechanical properties of lightweight concrete relative to normalweight concrete of the same compressive strength.

$$l : \underline{1.00}$$

$f$ : Strength reduction factor.

$$f : \underline{0.60}$$

### Minimum transverse reinforcement (ACI 318M-14, 11.6)

The worst case forces to be withstood from the analysis are produced at Elevation 7.00 (Base), in the combination of loadcase 1.2·PP+1.2·CM-0.3·SX-SY.

If in-plane  $V_u > 0.5 \cdot \phi V_c$ , shall be satisfied:

$$\rho_t \geq 0.0025$$

$$0.0029 \geq 0.0025 \quad \checkmark$$

Where:

$r_t$ : Ratio of area of distributed transverse reinforcement to gross concrete area perpendicular to that reinforcement.

$$r_t : \frac{0.0029}{}$$

$V_u$ : Factored shear force at section.

$$V_u : \frac{1614.3}{\text{kN}}$$

$V_c$ : Nominal shear strength provided by concrete.

$$V_c : \frac{2929.8}{\text{kN}}$$

### Minimum longitudinal reinforcement (ACI 318M-14, 11.6)

The worst case forces to be withstood from the analysis are produced at Elevation 7.00 (Base), in the combination of loadcase 1.2·PP+1.2·CM-0.3·SX-SY.

If in-plane  $V_u > 0.5 \cdot \phi V_c$ , shall be satisfied:

$$\rho_l \geq 0.0025 + 0.5(2.5 - h_w / l_w)(\rho_t - 0.0025)$$

$$0.0029 \geq 0.0028 \quad \checkmark$$

$$\rho_l \geq 0.0025$$

$$0.0029 \geq 0.0025 \quad \checkmark$$

Where:

$r_l$ : Ratio of area of distributed longitudinal reinforcement to gross concrete area perpendicular to that reinforcement.

$$r_l : \frac{0.0029}{}$$

$r_t$ : Ratio of area of distributed transverse reinforcement to gross concrete area perpendicular to that reinforcement.

$$r_t : \frac{0.0029}{}$$

$V_u$ : Factored shear force at section.

$$V_u : \frac{1614.3}{\text{kN}}$$

$V_c$ : Nominal shear strength provided by concrete.

$$V_c : \frac{2929.8}{\text{kN}}$$

$h_w$ : Height of wall.

$$h_w : \frac{350.0}{}$$

$l_w$ : Length of wall.

$$l_w : \frac{500.0}{}$$

### Maximum spacing of transverse reinforcement (ACI 318M-14, 11.7.3)

The worst case forces to be withstood from the analysis are produced at Elevation 7.00 (Base), in the combination of loadcase 1.4·PP+1.4·CM.

If in-plane  $V_u \leq 0.5 \cdot \phi V_c$ , shall be satisfied:

$$s \leq \min(3h, 450 \text{ mm})$$

$$30.0 \text{ cm} \leq 45.0 \text{ cm} \quad \checkmark$$

Where:

s: Spacing of transverse bars.

$$s : \frac{30.0}{\text{cm}}$$

h: Thickness of wall.

$$h : \frac{30.0}{\text{cm}}$$

$V_u$ : Factored shear force at section.

$$V_u : \frac{0.0}{\text{kN}}$$

$V_c$ : Nominal shear strength provided by concrete.

$$V_c : \frac{644.4}{\text{kN}}$$

### Maximum spacing of longitudinal reinforcement (ACI 318M-14, 11.7.2)

The worst case forces to be withstood from the analysis are produced at Elevation 7.00 (Base), in the combination of loadcase 1.4·PP+1.4·CM.

If in-plane  $V_u \leq 0.5 \cdot \phi V_c$ , shall be satisfied:

$$s \leq \min(3h, 450 \text{ mm})$$

$$30.0 \text{ cm} \leq 45.0 \text{ cm} \quad \checkmark$$

Where:

s: Spacing of longitudinal bars.

$$s : \frac{30.0}{\text{cm}}$$

h: Thickness of wall.

$$h : \frac{30.0}{\text{cm}}$$

$V_u$ : Factored shear force at section.

$$V_u : \frac{0.0}{\text{kN}}$$

$V_c$ : Nominal shear strength provided by concrete.

$$V_c : \frac{644.4}{\text{kN}}$$

### Number of layers (ACI 318M-14, 11.7.2.3)

For walls with 'h' greater than 250 mm distributed reinforcement for each direction shall be placed in two layers parallel with wall faces. ✓

h: Thickness of wall.

h : 30.0 cm

n: Number of layers.

n : 2

ACI 318M-14, Work section 18

### Distributed web reinforcement ratios (ACI 318M-14, 18.10.2.1)

The worst case forces to be withstood from the analysis are produced at Elevation 7.00 (Base), in the combination of loadcase 1.2·PP+1.2·CM+0.3·SX+SY.

If in-plane  $V_u \leq 0.083A_{cv}\lambda\sqrt{f'_c}$ , shall be satisfied:

$$\rho_l \geq 0.0025 + 0.5(2.5 - h_w / l_w)(\rho_t - 0.0025)$$

$$0.0029 \geq 0.0028 \quad \checkmark$$

$$\rho_t \geq 0.0025$$

$$0.0029 \geq 0.0025 \quad \checkmark$$

Where:

$\rho_l$ : Ratio of area of distributed longitudinal reinforcement to gross concrete area perpendicular to that reinforcement.

$$\rho_l : \underline{0.0029}$$

$\rho_t$ : Ratio of area of distributed transverse reinforcement to gross concrete area perpendicular to that reinforcement.

$$\rho_t : \underline{0.0029}$$

$V_u$ : Factored shear force at section.

$$V_u : \underline{-1614.3} \text{ kN}$$

$A_{cv}$ : Area of concrete section.

$$A_{cv} : \underline{1500000.00} \text{ mm}^2$$

$f'_c$ : Specified compressive strength of concrete.

$$f'_c : \underline{35.00} \text{ MPa}$$

$$\sqrt{f'_c} \leq 8.3 \text{ MPa}$$

$l$ : Modification factor to reflect the reduced mechanical properties of lightweight concrete relative to normalweight concrete of the same compressive strength.

$$l : \underline{1.00}$$

### Maximum reinforcement spacing (ACI 318M-14, 18.10.2.1)

Required:

$$s_l \leq 450 \text{ mm}$$

$$30.0 \text{ cm} \leq 45.0 \text{ cm} \quad \checkmark$$

$$s_t \leq 450 \text{ mm}$$

$$30.0 \text{ cm} \leq 45.0 \text{ cm} \quad \checkmark$$

$s_l$ : Spacing of longitudinal bars.

$$s_l : \underline{30.0} \text{ cm}$$

$s_t$ : Spacing of transverse bars.

$$s_t : \underline{30.0} \text{ cm}$$

### Number of layers (ACI 318M-14, 18.10.2.2)

At least two curtains of reinforcement shall be used in a wall if  $V_u > 0.17A_{cv}\lambda\sqrt{f'_c}$  or  $h_w/l_w \geq 2.0$  ✓

n: Number of layers.

$$n : \underline{2}$$

$V_u$ : Factored shear force at section.

$$V_u : \underline{0.0} \text{ kN}$$

$A_{cv}$ : Area of concrete section.

$$A_{cv} : \underline{1500000.00} \text{ mm}^2$$

$l$ : Modification factor to reflect the reduced mechanical properties of lightweight concrete relative to normalweight concrete of the same compressive strength.

$$l : \underline{1.00}$$

$f'_c$ : Specified compressive strength of concrete.

$$f'_c : \underline{35.00} \text{ MPa}$$

$h_w$ : Height of wall.

$$h_w : \underline{350.0} \text{ cm}$$

$l_w$ : Length of wall.

$$l_w : \underline{500.0} \text{ cm}$$

### Shear strength (ACI 318M-14, 18.10.4.1)

The worst case forces to be withstood from the analysis are produced at Elevation 7.00 (Base), in the combination of loadcase 1.2·PP+1.2·CM+0.5·Qa-0.3·SX-SY.

$$\phi V_n \geq V_u$$

$$2415.0 \text{ kN} \geq 1626.3 \text{ kN} \quad \checkmark$$

Where:

$V_u$ : Factored shear force at section.

$$V_u : \frac{1626.3}{\quad} \text{ kN}$$

$V_n$ : Nominal shear strength.

$$V_n : \frac{4025.0}{\quad} \text{ kN}$$

$$V_n = A_{cv} \left( \alpha_c \lambda \sqrt{f'_c} + \rho_t f_y \right)$$

$$V_n \leq 0.83 A_{cv} \sqrt{f'_c} \quad (18.10.4.4)$$

$A_{cv}$ : Area of concrete section.

$$A_{cv} : \frac{1500000.00}{\quad} \text{ mm}^2$$

The coefficient  $\alpha_c$  is 0.25 for  $h_w/l_w \leq 1.50$ , is 0.17 for  $h_w/l_w \geq 2.00$ , and varies linearly between 0.25 and 0.17 for  $h_w/l_w$  between 1.50 and 2.00.

$$a_c : \frac{0.25}{\quad}$$

$h_w$ : Height of wall.

$$h_w : \frac{350.0}{\quad} \text{ cm}$$

$l_w$ : Length of wall.

$$l_w : \frac{500.0}{\quad} \text{ cm}$$

$l$ : Modification factor to reflect the reduced mechanical properties of lightweight concrete relative to normalweight concrete of the same compressive strength.

$$l : \frac{1.00}{\quad}$$

$f'_c$ : Specified compressive strength of concrete.

$$f'_c : \frac{35.00}{\quad} \text{ MPa}$$

$r_t$ : Ratio of area of distributed transverse reinforcement to gross concrete area perpendicular to that reinforcement.

$$r_t : \frac{0.0029}{\quad}$$

$f_y$ : Specified yield strength of transverse reinforcement.

$$f_y : \frac{420.00}{\quad} \text{ MPa}$$

$\phi$ : Strength reduction factor.

$$\phi : \frac{0.60}{\quad}$$

### Longitudinal reinforcement ratio (ACI 318M-14, 18.10.4.3)

If  $h_w/l_w$  does not exceed 2.00, reinforcement ratio  $\rho_l$  shall be at least the reinforcement ratio  $\rho_t$ .

$$\rho_l \geq \rho_t$$

$$0.0029 \geq 0.0029 \quad \checkmark$$

Where:

$\rho_l$ : Ratio of area of distributed longitudinal reinforcement to gross concrete area perpendicular to that reinforcement.

$$\rho_l : \frac{0.0029}{\quad}$$

$\rho_t$ : Ratio of area of distributed transverse reinforcement to gross concrete area perpendicular to that reinforcement.

$$\rho_t : \frac{0.0029}{\quad}$$

$$h_w/l_w : \frac{0.70}{\quad}$$

### Edge elements (ACI 318M-14, 18.10.6.1, 18.10.6.5) (Initial)

Special boundary elements

Structural wall shall have special boundary elements at boundaries and edges around openings where the maximum extreme fiber compressive stress,  $\sigma$ , exceeds  $0.2f'_c$ :

(ACI 318M-14, 18.10.6.3)

$P_u$ (kN)	$M_u$ (kN·m)	Edge elements	Location	$\sigma$ (MPa)	$0.2f'_c$ (MPa)	Necesita elemento especial
4858.1	-4808.2	1.2·PP+1.2·CM+0.5·Qa-0.3·SX+SY	Elevation 7.00 (Base)	7.09	7.00	Yes

Where:

$P_u$ : Factored axial force.

$M_u$ : Factored moment.

$\sigma$ : Maximum extreme fiber compressive stress.

$f'_c$ : Specified compressive strength of concrete.

### Edge elements (ACI 318M-14, 18.10.6.1, 18.10.6.5) (Final)

#### Special boundary elements

Structural wall shall have special boundary elements at boundaries and edges around openings where the maximum extreme fiber compressive stress,  $\sigma$ , exceeds  $0.2f'_c$ :

(ACI 318M-14, 18.10.6.3)

$P_u$ (kN)	$M_u$ (kN·m)	Edge elements	Location	$\sigma$ (MPa)	$0.2f'_c$ (MPa)	Necesita elemento especial
5547.8	4877.2	1.2·PP+1.2·CM+0.5·Qa-0.3·SX-SY	Elevation 7.00 (Base)	7.60	7.00	Yes

Where:

$P_u$ : Factored axial force.

$M_u$ : Factored moment.

s: Maximum extreme fiber compressive stress.

$f'_c$ : Specified compressive strength of concrete.

### Length of boundary element (ACI 318M-14, 18.10.6.4(a)) (Initial)

The worst case forces to be withstood from the analysis are produced at Elevation 7.00 (Base), in the combination of loadcase 1.2·PP+1.2·CM+0.5·Qa-0.3·SX+SY.

The boundary element shall extend horizontally from the extreme compression fiber a distance at least the greater of  $(c-0.1l_w)$  and  $c/2$ .

$$l_{be} \geq \text{MAX}(c - 0.1l_w, c/2) \quad 60.0 \geq 43.1 \quad \checkmark$$

Where:

$l_{be}$ : Length of boundary element

$$l_{be} : \underline{60.0} \text{ cm}$$

c: Largest neutral axis depth calculated for the factored axial force and nominal moment strength.

$$c : \underline{86.2} \text{ cm}$$

$l_w$ : Length of wall.

$$l_w : \underline{500.0} \text{ cm}$$

$P_u$ : Factored axial force.

$$P_u : \underline{4858.1} \text{ kN}$$

$M_n$ : Nominal moment strength.

$$M_n : \underline{-18771.2} \text{ kN·m}$$

### Length of boundary element (ACI 318M-14, 18.10.6.4(a)) (Final)

The worst case forces to be withstood from the analysis are produced at Elevation 7.00 (Base), in the combination of loadcase 1.2·PP+1.2·CM+0.5·Qa-0.3·SX-SY.

The boundary element shall extend horizontally from the extreme compression fiber a distance at least the greater of  $(c-0.1l_w)$  and  $c/2$ .

$$l_{be} \geq \text{MAX}(c - 0.1l_w, c/2) \quad 60.0 \geq 45.7 \quad \checkmark$$

Where:

$l_{be}$ : Length of boundary element

$$l_{be} : \underline{60.0} \text{ cm}$$

c: Largest neutral axis depth calculated for the factored axial force and nominal moment strength.

$$c : \underline{91.3} \text{ cm}$$

$l_w$ : Length of wall.

$$l_w : \underline{500.0} \text{ cm}$$

$P_u$ : Factored axial force.

$$P_u : \underline{5547.8} \text{ kN}$$

$M_n$ : Nominal moment strength.

$$M_n : \underline{20082.7} \text{ kN·m}$$

### Maximum spacing of longitudinal bars laterally supported (ACI 318M-14, 18.10.6.4(e), 18.7.5.2) (Initial)

$$h_x \leq \text{MIN}\left(\frac{2}{3}b, 350\text{mm}\right) \quad 15.0 \leq 20.0 \quad \checkmark$$

Where:

b: Width of boundary element

$$b : \underline{30.0} \text{ cm}$$

$h_x$ : Spacing of the longitudinal bars that are supported laterally by the corner of a supplementary hook or closed confinement stirrup branch.

$$h_x : \underline{15.0} \text{ cm}$$

Maximum spacing of longitudinal bars laterally supported (ACI 318M-14, 18.10.6.4(e), 18.7.5.2) (Final)

$$h_x \leq \text{MIN} \left( \frac{2}{3}b, 350\text{mm} \right) \quad 15.0 \leq 20.0 \quad \checkmark$$

Where:

b: Width of boundary element b : 30.0 cm  
 h<sub>x</sub>: Spacing of the longitudinal bars that are supported laterally by the corner of a supplementary hook or closed confinement stirrup branch. h<sub>x</sub> : 15.0 cm

Width of boundary element (ACI 318M-14, 18.10.6.4(b)) (Initial)

Width of the flexural compression zone, 'b', including flange, if present, shall be:

$$b \geq h_u / 16 \quad 30.0 \geq 21.9 \text{ cm} \quad \checkmark$$

When  $h_w/l_w \geq 2.0$  and  $c/l_w \geq 3/8$

$$b \geq 300\text{mm} \quad \text{--} \quad \checkmark$$

Where:

h<sub>u</sub>: Laterally unsupported height at extreme compression fiber of wall. h<sub>u</sub> : 350.0 cm  
 l<sub>w</sub>: Length of wall. l<sub>w</sub> : 500.0 cm  
 h<sub>w</sub>: Height of wall. h<sub>w</sub> : 350.0 cm  
 c: Distance from extreme compression fiber to neutral axis. c : 86.2 cm

Width of boundary element (ACI 318M-14, 18.10.6.4(b)) (Final)

Width of the flexural compression zone, 'b', including flange, if present, shall be:

$$b \geq h_u / 16 \quad 30.0 \geq 21.9 \text{ cm} \quad \checkmark$$

When  $h_w/l_w \geq 2.0$  and  $c/l_w \geq 3/8$

$$b \geq 300\text{mm} \quad \text{--} \quad \checkmark$$

Where:

h<sub>u</sub>: Laterally unsupported height at extreme compression fiber of wall. h<sub>u</sub> : 350.0 cm  
 l<sub>w</sub>: Length of wall. l<sub>w</sub> : 500.0 cm  
 h<sub>w</sub>: Height of wall. h<sub>w</sub> : 350.0 cm  
 c: Distance from extreme compression fiber to neutral axis. c : 91.3 cm

Spacing of transverse reinforcement of boundary element (ACI 318M-14, 18.10.6.4(e), 18.7.5.3) (Initial)

Spacing of transverse reinforcement shall not exceed:

$$s \leq \frac{\min(b, l_{be})}{3} \quad 9.0 \leq 10.0 \text{ cm} \quad \checkmark$$

$$s \leq 6 \cdot d_{b,\min} \quad 9.0 \leq 9.5 \text{ cm} \quad \checkmark$$

$$s \leq s_0 \quad 9.0 \leq 15.0 \text{ cm} \quad \checkmark$$

Where:

b: Width of boundary element b : 30.0 cm  
 l<sub>be</sub>: Length of boundary element l<sub>be</sub> : 60.0 cm  
 d<sub>b,min</sub>: Diameter of the smallest longitudinal bar. d<sub>b,min</sub> : 1.6 cm  
 s: Center-to-center spacing of transverse reinforcement. s : 9.0 cm  
 h<sub>x</sub>: Maximum center-to-center spacing of longitudinal bars laterally supported by corners of crossties or hoop legs around the perimeter of the column. h<sub>x</sub> : 15.0 cm  
 s<sub>0</sub>: Maximum separation s<sub>0</sub> : 15.0 cm

$$s_0 \leq 100 + \left( \frac{350 - h_x}{3} \right), s_0 \leq 150 \text{ mm}$$

Spacing of transverse reinforcement of boundary element (ACI 318M-14, 18.10.6.4(e), 18.7.5.3) (Final)

Spacing of transverse reinforcement shall not exceed:

$$s \leq \frac{\min(b, l_{be})}{3} \quad 9.0 \leq 10.0 \text{ cm} \quad \checkmark$$

$$s \leq 6 \cdot d_{b,min} \quad 9.0 \leq 9.5 \text{ cm} \quad \checkmark$$

$$s \leq s_0 \quad 9.0 \leq 15.0 \text{ cm} \quad \checkmark$$

Where:

b: Width of boundary element	b : <u>30.0</u> cm
$l_{be}$ : Length of boundary element	$l_{be}$ : <u>60.0</u> cm
$d_{b,min}$ : Diameter of the smallest longitudinal bar.	$d_{b,min}$ : <u>1.6</u> cm
s: Center-to-center spacing of transverse reinforcement.	s : <u>9.0</u> cm
$h_x$ : Maximum center-to-center spacing of longitudinal bars laterally supported by corners of crossties or hoop legs around the perimeter of the column.	$h_x$ : <u>15.0</u> cm
$s_0$ : Maximum separation	$s_0$ : <u>15.0</u> cm

$$s_0 \leq 100 + \left( \frac{350 - h_x}{3} \right), s_0 \leq 150 \text{ mm}$$

Amount of transverse reinforcement of boundary element (ACI 318M-14, 18.10.6.4(f)) (Initial)

The amount of transverse reinforcement shall be in accordance with:

$$A_{sh} \geq 0.3 \left( \frac{A_g}{A_{ch}} - 1 \right) \frac{f'_c}{f_{yt}} \cdot s \cdot b_c \quad 283.87 \geq 170.53 \text{ mm}^2 \quad \checkmark$$

$$A_{sh} \geq 0.09 \frac{f'_c}{f_{yt}} \cdot s \cdot b_c \quad 283.87 \geq 162.00 \text{ mm}^2 \quad \checkmark$$

Where:

$A_{sh}$ : Total cross-sectional area of transverse reinforcement, including crossties, within spacing s and perpendicular to dimension, $b_c$ .	
$A_g$ : Gross area of concrete section.	$A_g$ : <u>180000.00</u> mm <sup>2</sup>
$A_{ch}$ : Cross-sectional area measured to the outside edges of transverse reinforcement.	$A_{ch}$ : <u>136800.00</u> mm <sup>2</sup>
$b_c$ : Cross-sectional dimension of member core measured to the outside edges of the transverse reinforcement composing area $A_{sh}$ .	$b_c$ : <u>24.0</u> cm
s: Center-to-center spacing of transverse reinforcement.	s : <u>9.0</u> cm
$f'_c$ : Specified compressive strength of concrete.	$f'_c$ : <u>35.00</u> MPa
$f_{yt}$ : Specified yield strength of transverse reinforcement.	$f_{yt}$ : <u>420.00</u> MPa

Amount of transverse reinforcement of boundary element (ACI 318M-14, 18.10.6.4(f)) (Final)

The amount of transverse reinforcement shall be in accordance with:

$$A_{sh} \geq 0.3 \left( \frac{A_g}{A_{ch}} - 1 \right) \frac{f'_c}{f_{yt}} \cdot s \cdot b_c \quad 283.87 \geq 170.53 \text{ mm}^2 \quad \checkmark$$

$$A_{sh} \geq 0.09 \frac{f'_c}{f_{yt}} \cdot s \cdot b_c \quad 283.87 \geq 162.00 \text{ mm}^2 \quad \checkmark$$

Where:

$A_{sh}$ : Total cross-sectional area of transverse reinforcement, including crossties, within spacing s and perpendicular to dimension, $b_c$ .	
$A_g$ : Gross area of concrete section.	$A_g$ : <u>180000.00</u> mm <sup>2</sup>
$A_{ch}$ : Cross-sectional area measured to the outside edges of transverse reinforcement.	$A_{ch}$ : <u>136800.00</u> mm <sup>2</sup>
$b_c$ : Cross-sectional dimension of member core measured to the outside edges of the transverse reinforcement composing area $A_{sh}$ .	$b_c$ : <u>24.0</u> cm
s: Center-to-center spacing of transverse reinforcement.	s : <u>9.0</u> cm
$f'_c$ : Specified compressive strength of concrete.	$f'_c$ : <u>35.00</u> MPa

$f_{yt}$ : Specified yield strength of transverse reinforcement.

$f_{yt}$  : 420.00 MPa